

10/11/2018

Recap

RANS : $\tilde{u}_i = U_i + u_i$

$$\frac{D}{Dt} U_i = \dots - \frac{\partial}{\partial x_j} \overline{u_i u_j} + \dots$$

$$\frac{D}{Dt} \overline{u_i u_j} = \dots - \frac{\partial}{\partial x_k} \overline{u_i u_j u_k} + \dots$$

Turbulence Closure Problem $\rightarrow$ Model

$$\overline{u_i u_j} = \frac{2}{3} k S_{ij} = 2 \nu_t S_{ij}$$

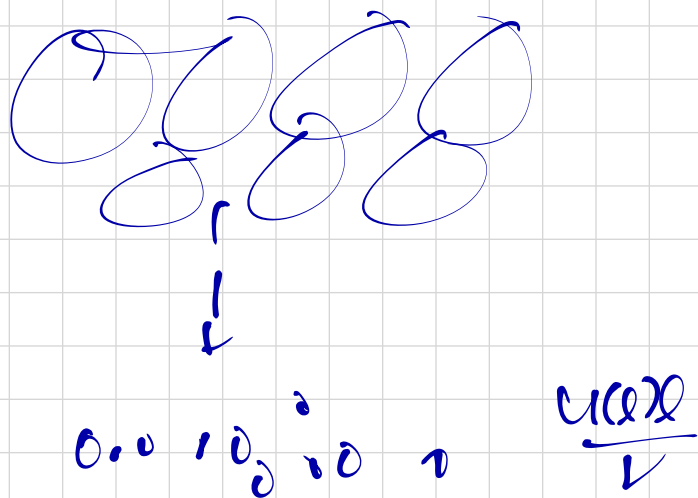
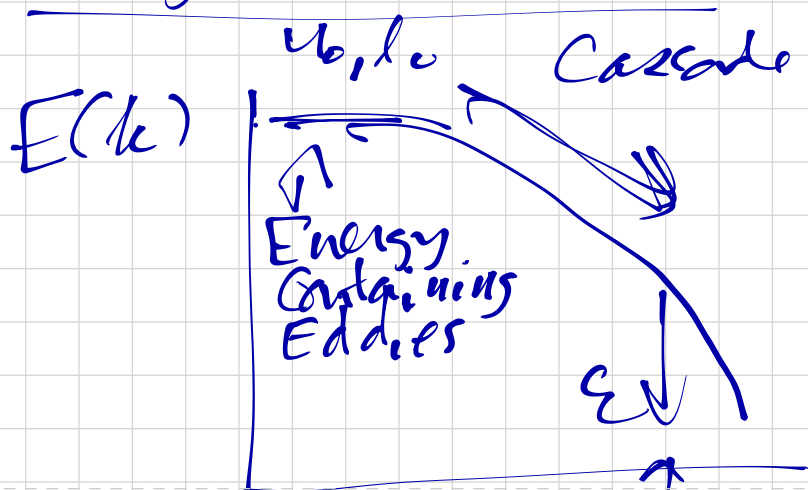
$$\frac{D}{Dt} \underbrace{\overline{u_i u_i}}_k = - \underbrace{\overline{u_i u_j} S_{ij}}_{\text{Production terms}}$$

Simple Shear Flows

$$\begin{aligned} \frac{D}{Dt} \overline{u_1^2} &= -\overline{u_1 u_2} \frac{\partial U_1}{\partial x_2} + \overline{p \frac{\partial u_1}{\partial x_1}} + \dots \\ \overline{u_2^2} &= 0 + \overline{p \frac{\partial u_2}{\partial x_2}} + \dots \\ \overline{u_3^2} &= 0 + \overline{p \frac{\partial u_3}{\partial x_3}} + \dots \end{aligned}$$

Inter component transfer

Energy Cascade



$$\epsilon \sim \frac{u_0^3}{l_0} \quad \text{Dissipating Eddies}$$

Local Isotropy

Small scale $l \ll l_0$ isotropic

$$l < l_{EI}$$

isotropic

$$l > l_{EC}$$

anisotropic

$$\tau_{\text{small}} \ll \tau_{\text{energy containing}}$$

$$\frac{dk}{dt} = -\epsilon$$

Kolmogorov 1st Similarity

During the cascade process, all information about the geometry of large eddies is lost

→ Statistics of small scale have a universal form, i.e., similar, in any high Re flows, and it is uniquely determined by ν and ϵ . Small scales receive energy from large eddies, and dissipates the energy.

$l < l_{EI}$ is referred to as universal equilibrium range.

$$\tau(l) = \frac{l}{u(l)} \text{ is small (compared to } l_0/u_0)$$

such that small eddies adapt quickly to
dynamic equilibrium with the

maintain a balance between the energy transfer imposed by the large eddies.

$$\eta = \nu^a \varepsilon^b = \left(\frac{L^2}{T}\right)^a \left(\frac{L^2}{T^3}\right)^b$$

$$\begin{aligned} L: 2a + 2b &= 1 \\ T: -a - 3b &= 0 \end{aligned} \rightarrow a = \frac{3}{4}, b = -\frac{1}{4}$$

$$\eta = \left(\nu^3 / \varepsilon\right)^{1/4}$$

Kolmogorov length scales.

On the average, the smallest length scale in turbulent flows.

$$u_\eta = (\varepsilon \nu)^{1/4}$$

$$\tau_\eta = (\nu / \varepsilon)^{1/2}$$

Note : 1. $Re_\eta = \frac{u_\eta \eta}{\nu} = 1$

2. $\varepsilon = 2\nu \overline{s_{ij}s_{ij}}$

$$\sim \nu \left(\frac{u_\eta}{\eta}\right)^2 = \nu / \tau_\eta^2$$

$$\frac{u_\eta}{\eta} = \frac{1}{\tau_\eta}$$

time scale associated with the dissipation

"Similarity" or "universal"

$$\underline{y} = (\underline{x} - \underline{x}_0) / \eta, \quad w(\underline{y}) = [\underline{u}(\underline{x}) - \underline{u}(\underline{x}_0)] / u_\eta$$

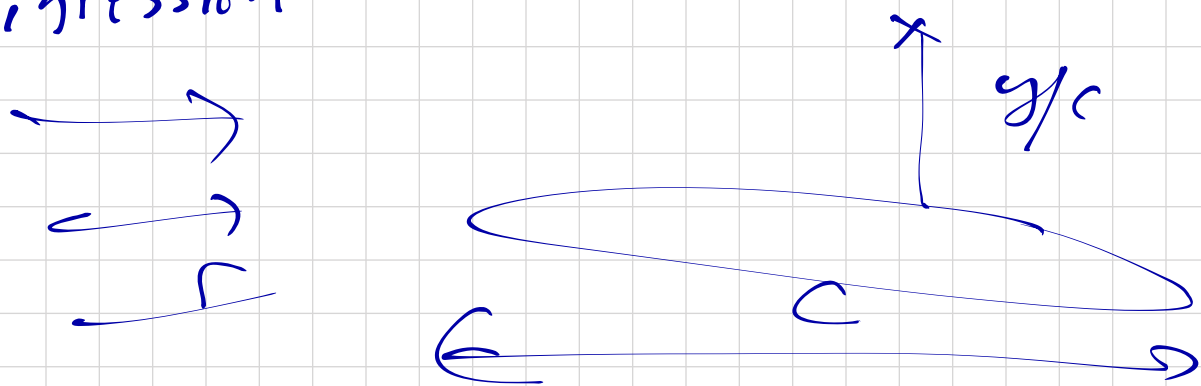
For $|\underline{y}| < \frac{L\varepsilon}{\eta}$

$$\begin{matrix} \varepsilon & \nu \\ \uparrow & \uparrow \end{matrix}$$

$$\varepsilon \sim \frac{L^2}{T^3}$$

$$\nu \sim L^2 / T$$

Dissipation

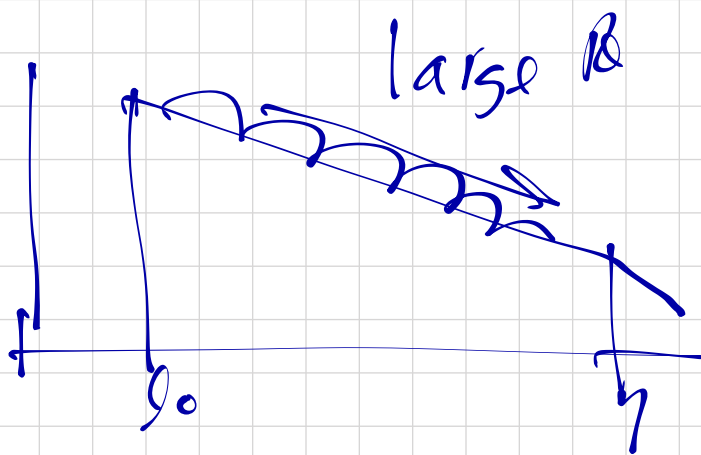
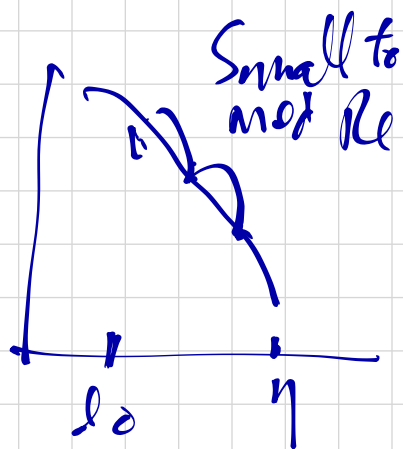


Statistics indep. of ε and ν ($\therefore$ cannot construct a non-dim out of ε and ν)

$\rightarrow$ Similar!

$$\text{Also } \frac{\eta}{l_0} = \left(\frac{\nu^3}{\varepsilon l_0^4} \right)^{1/4} = \left(\frac{\nu^3}{u_0^3 l_0^3} \right)^{1/4} = \left(\frac{\nu}{u_0 l_0} \right)^{3/4} = Re^{-3/4}$$

$$\frac{l_0}{\eta} = Re^{3/4}$$



Similarly

$$\frac{u_\eta}{u_0} \sim Re^{-1/4}, \quad \frac{\tau_\eta}{\tau_0} \sim Re^{-1/2}$$

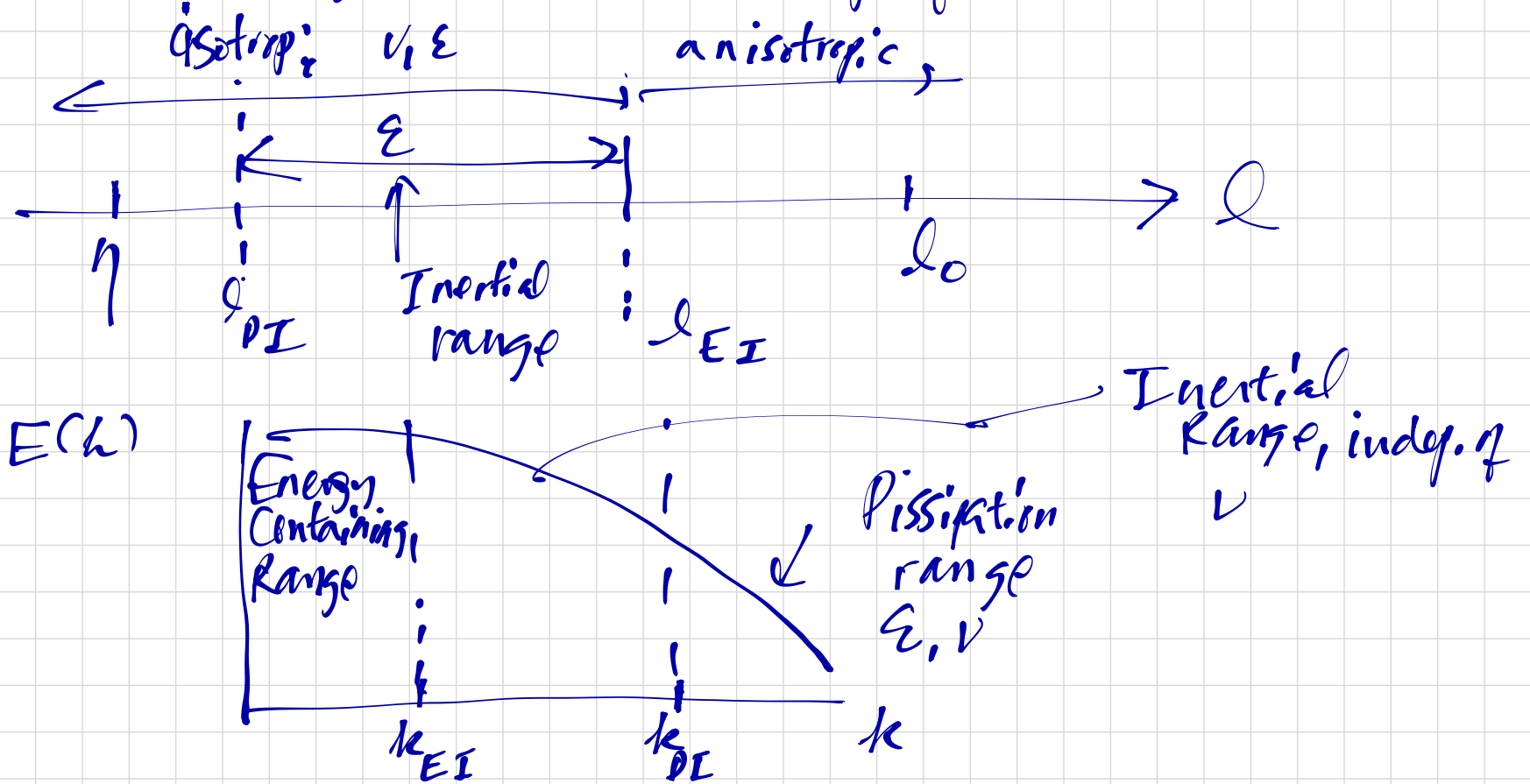
Show images
for large Re

Kolmogorov 2nd Similarity

At sufficiently large Re $\eta \ll l \ll l_0$

The statistics of the velocity

The statistics of the motion x have a universal form indep. of ν



Inertial range

$$u(l) = (\epsilon l)^{1/3} = u_\eta \left(\frac{l}{\eta}\right)^{1/3} = u_0 \left(\frac{l}{l_0}\right)^{1/3}$$

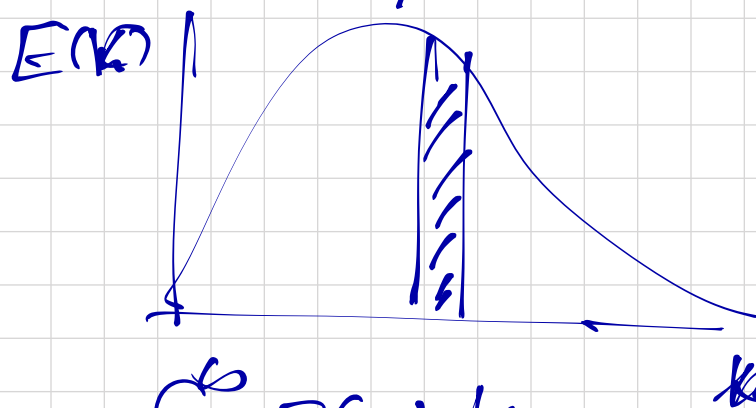
$$\tau(l) = (l^2 / \epsilon)^{1/3} = \tau_\eta \left(\frac{l}{\eta}\right)^{2/3} = \tau_0 \left(\frac{l}{l_0}\right)^{2/3}$$

Thus $l \downarrow \quad u(l), \tau(l) \downarrow$

The energy trans-fer rate T_{EI} in the inertial range

$$T_{EI} \sim \frac{u(l)^2}{\tau(l)} = \frac{(\epsilon l)^{2/3}}{(l^2 / \epsilon)^{1/3}} = \epsilon$$

Energy Spectrum Function, $E(k)$ $k = |k|$



$$TKE = k = \frac{1}{2} \overline{u_i u_i} = \int_0^\infty E(k) dk$$

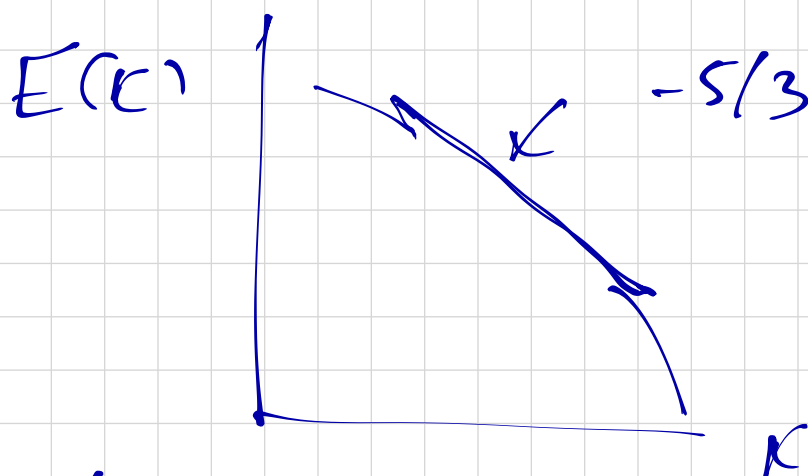
$$E(k) \stackrel{D}{=} \frac{V_0^2}{L^3} = \frac{L^3}{T^2}$$

$$E(k) = C \epsilon^m k^n$$

$$\rightarrow m = 2/3 \quad n = -5/3$$

$$E(k) = C \epsilon^{2/3} k^{-5/3} \quad \text{"-5/3 law"}$$

~ 1.5
Kolmogorov
Const.



Recall 1-D Spectra

$$\Phi_{ij}(\underline{k}) = -$$

$$\left\{ \begin{array}{l} \phi_{11} \\ R_{11} \end{array} \right. = \frac{1}{2\pi} \int R_{11}(r_1, 0, r) e^{-ik_1 r_1} dr_1$$

In general, the relationship between ϕ_{11} and $E(k)$ very complicated. For isotropic turbulence,

$$E_{11} \triangleq 2\phi_{11}(k_1)$$

$$E(k) = \frac{1}{2} k^3 \frac{d}{dk} \left(\frac{1}{k} \frac{dE_{11}}{dk} \right)$$

$$E_{22}(k_1) = \frac{1}{2} \left(E_{11} - k_1 \frac{d}{dk_1} E_{11} \right)$$

$$E(k) \sim k^m \rightarrow E_{11}, E_{22} \sim k_1^m$$

Inertial range

$$E(k) = C \varepsilon^{2/3} k^{-5/3}$$

$$E_{11}(k_1) = C_1 \varepsilon^{2/3} k_1^{-5/3}$$

$$E_{22}(k_2) = C_2 \varepsilon^{2/3} k_2^{-5/3}$$

all have "-5/3" slope

$$C \sim 1.5$$

$$C_1 \sim 0.49$$

$$C_2 = \frac{4}{3} C_1 \sim 0.65$$

$$So \quad E_{22} = \frac{4}{3} E_{11}$$

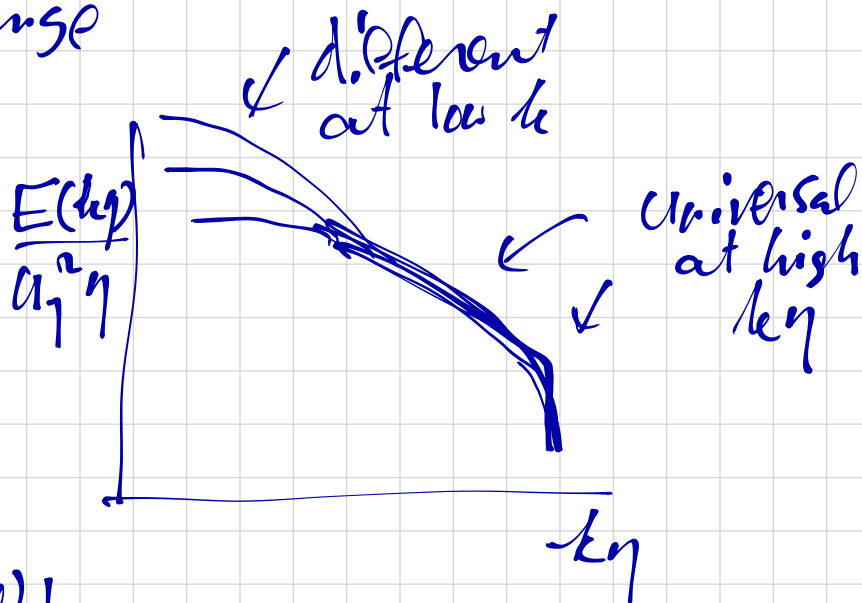
evidence for isotropy

Isotropic flows
 $\left(\frac{\partial u_i}{\partial x_i}\right)^2 = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_i}\right)^2$
 Only true when all scales are isotropic

At high k , dissipation range

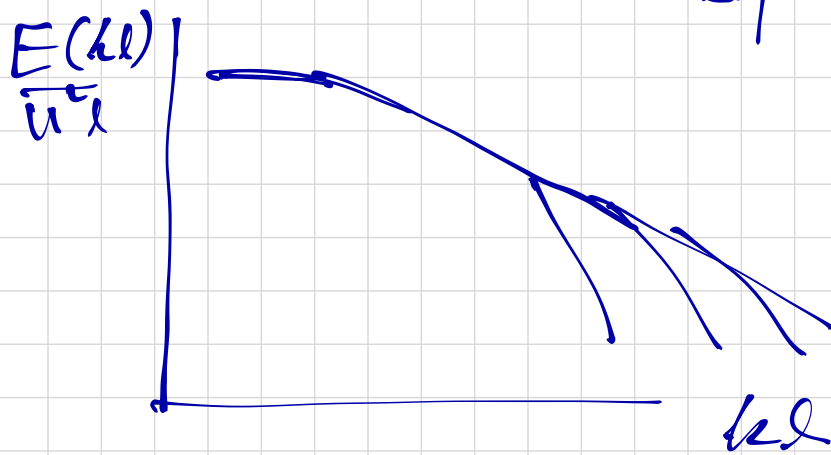
$$E(k) = E(k; \varepsilon, \nu)$$

$$\frac{E(k)}{u_\eta^2 \eta} = f(k\eta)$$



At low k

$$\frac{E(k)}{u^2 l} = F(kl)$$



In the overlap region

$$\frac{E}{u^2 l} = B (kl)^{-5/3}$$

$$E(kl) = B u^2 l k^{-5/3}$$

$$= B \left(\frac{u^3}{l}\right)^{2/3} k^{-5/3}$$

If you recall

$$E(kl) = C$$

From ~~the~~ ~~the~~

$$\epsilon = u^3/l \quad \text{ind. of } \nu$$

Rough estimation ϵ

$$\text{TBL} \quad \epsilon \sim u_{rms}^3 / \delta$$

Airbus cruising at 10,000 meter high.

$$M_\infty \sim 0.85$$

$$M_\infty = U_\infty / C$$

$$\nu = 3.5 \times 10^{-5} \text{ m}^2/\text{s}$$

$$C = 290 \text{ m/s}$$

$$\rightarrow U_\infty = 250 \text{ m/s} \quad (\sim 560 \text{ mph})$$

$$Re = \frac{U_\infty C_h}{\nu} = \frac{250 \text{ m/s} \cdot 5 \text{ m}}{3.5 \times 10^{-5} \text{ m}^2/\text{s}} = 3.5 \times 10^7$$

$$\delta = 0.37 l (Re)^{-0.2} \sim 5.7 \times 10^{-2} \text{ m} \quad \text{Integral Scale}$$

$$\epsilon \sim u^3/l = (25 \text{ m/s})^3 / 5.7 \times 10^{-2} \text{ m} = 2.74 \times 10^5 \text{ m}^2/\text{s}^3$$

$$\frac{u_{rms}}{U_\infty} \sim 0.1$$

$$u_{rms} = 25 \text{ m/s}$$

$$\eta = \left(\nu^3 / \epsilon \right)^{1/4} = 2 \times 10^{-5} \text{ m}$$

Kolmogorov scale

$$\epsilon = 15 \nu \left(\frac{\partial u_i}{\partial x_i} \right)^2 \sim 15 \nu \left(\frac{u}{l} \right)^2$$

$$\eta = \left(\frac{15 \nu u^2}{\epsilon} \right)^{\frac{1}{2}} = \boxed{10^{-3} \text{ m}} \quad \text{Taylor Micro Scale}$$

$$\eta < \lambda < \delta$$

TBL $\frac{\nu}{u_\tau}$

$$u_\tau = \sqrt{\frac{C_\tau}{2} u_\infty^2}$$

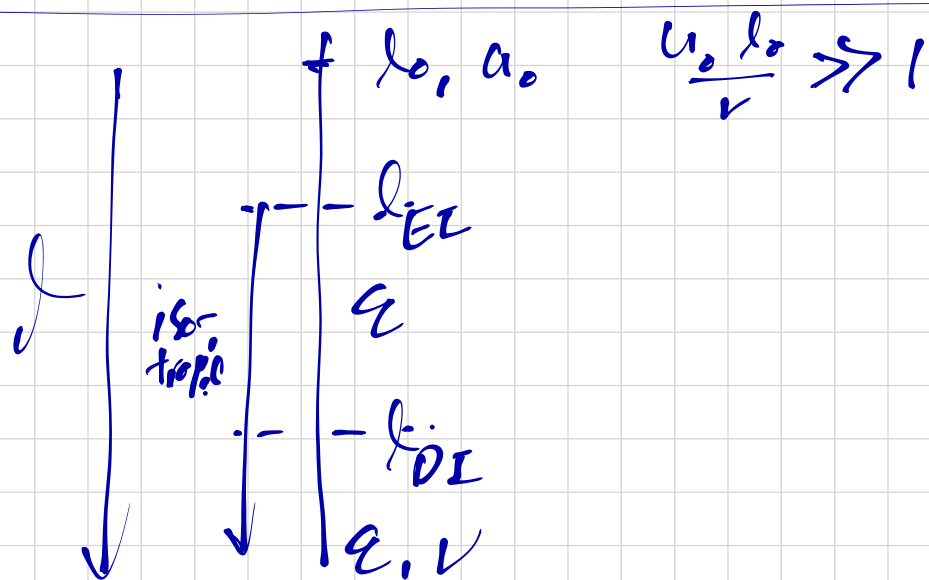
$\Rightarrow$

$$\frac{\nu}{u_\tau} = \boxed{4 \times 10^{-6} \text{ m}}$$

viscous wall scale

$$C_f = \frac{0.455}{(\log Re)^{2.55}} = 2.48 \times 10^{-3}$$

$\sim$ Kolmogorov scale



1941

1941b

Structure Function (Kolmogorov 1941b)

$$D_{ij}(\underline{r}, \underline{x}, t) = \frac{[\tilde{u}_i(\underline{x} + \underline{r}, t) - \tilde{u}_i(\underline{x}, t)]}{[\tilde{u}_j(\underline{x} + \underline{r}, t) - \tilde{u}_j(\underline{x}, t)]}$$

Local isotropy $|\underline{r}| \ll \mathcal{L}$

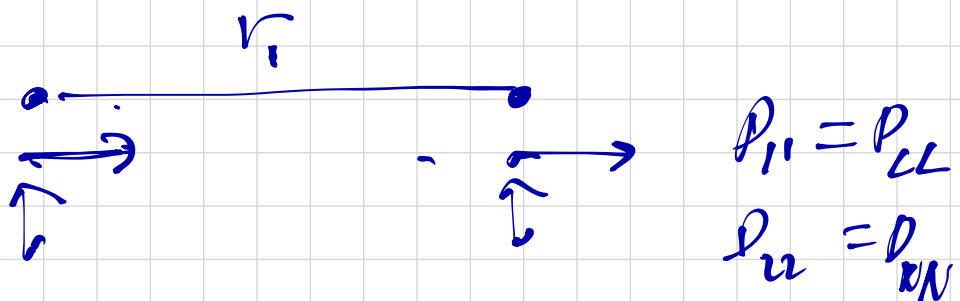
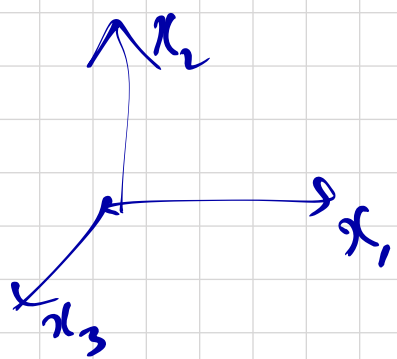
$D_{ij}(\underline{r}) \rightarrow \text{'isotrop.'}$

$$D_{ij} = A \delta_{ij} + B r_i r_j$$

General
2nd-order
isotropic tensor

P_{LL} : longitudinal structure function

P_{NN} : transverse " "



$$P_{ij} = \underbrace{P_{NN}}_A \delta_{ij} + \underbrace{[P_{LL} - P_{NN}]}_B \frac{1}{r^2} r_i r_j$$

Note

$$\frac{\partial}{\partial r_i} P_{ij} = 0$$

$$\frac{\partial}{\partial r_i} P_{ij} = \frac{r_j}{r^2} \left(r \frac{\partial}{\partial r} P_{LL} + 2(P_{LL} - P_{NN}) \right) = 0$$

$$\rightarrow P_{NN} = P_{LL} + \frac{1}{2} r \frac{\partial}{\partial r} P_{LL}$$

$\rightarrow P_{ij}$ is a function of P_{LL} alone for isotropic turbulence

$$P_{ij} = (\epsilon r)^{2/3} P_{LL} \left(\frac{r}{\eta} \right) \quad 1^{st} \text{ Similarity}$$

Inertial Range

$$P_{ij} = C_2 (\epsilon / r)^{2/3} \left(\frac{4}{3} \delta_{ij} - \frac{1}{3} \frac{r_i r_j}{r^2} \right)$$

Saddoughi & Veeravalli (JFM, 1994)

$$Re_S = 3.6 \times 10^6$$

$$S = 1.09 \text{ mm}$$

$$\eta = 0.09 \text{ mm}$$

$$\frac{S}{\eta} \approx 12,000$$

$$P_{11} / (\epsilon r)^{2/3} = C_2 \rightarrow 2.0$$

$$\rho_2 / (\epsilon_1)^{2/3} = \frac{4}{3} c_2$$